

**Cécile DEMAIN - Confidentiel** 

Simulation Engineer Part Simulation and Validation Laboratory POLYAMIDE Group Lyon Research and Technology Center

## **European Users Conference 2011**

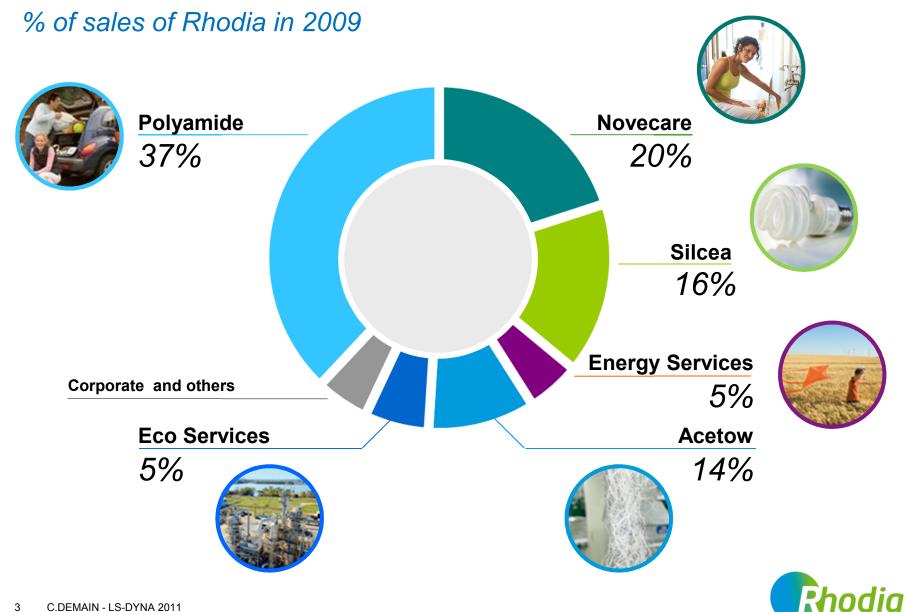
Improving the Prediction of LS-DYNA Calculations with Rhodia Data and Digimat

## Summary

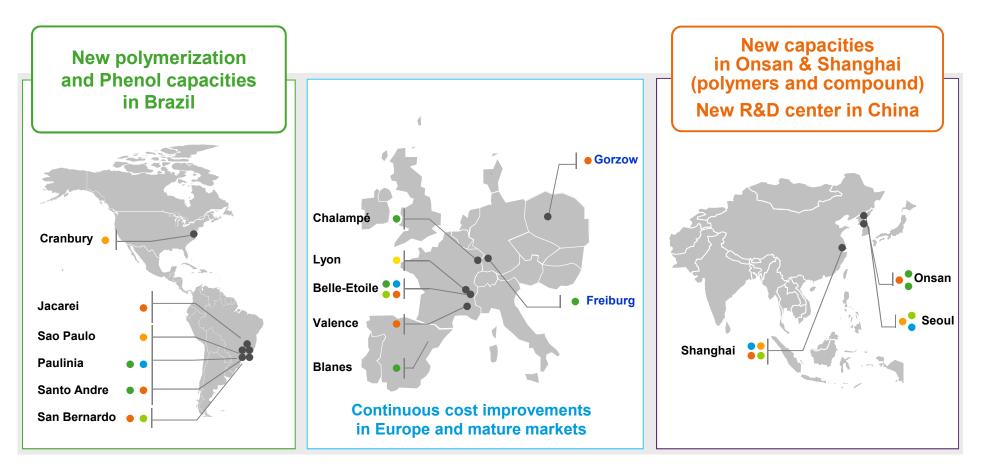
- RHODIA Polyamide
- MMI ConfidentDesign
  - Matrix behavior
  - Composite behavior
- Presentation of the MMI Beam
  - Injection & Microstructure
- Correlation using DIGIMAT to LS-DYNA
  - Material behavior
  - Model and results
- Conclusions



## **RHODIA : Six enterprises, leaders in their** markets



## **RHODIA Global presence**



- Worldwide Headquarter
- Application & Technology **Development Centre**

R&D Centers

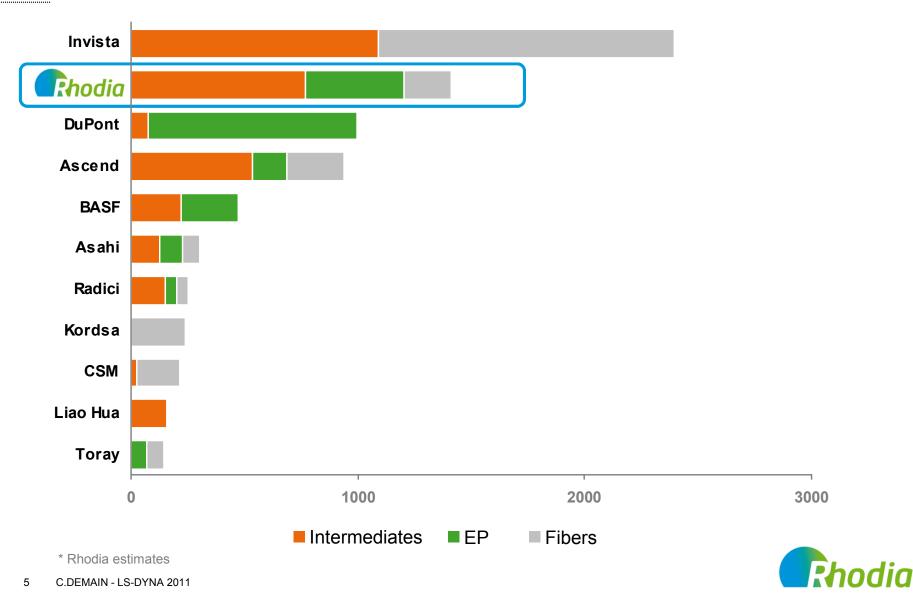
• Manufacturing Plant upstream

- Regional Headquarter
- Manufacturing Plant downstream



# RHODIA is the only fully integrated Polyamide 6.6 player with a strong position in Engineering Plastics

2008 Sales\* in €m





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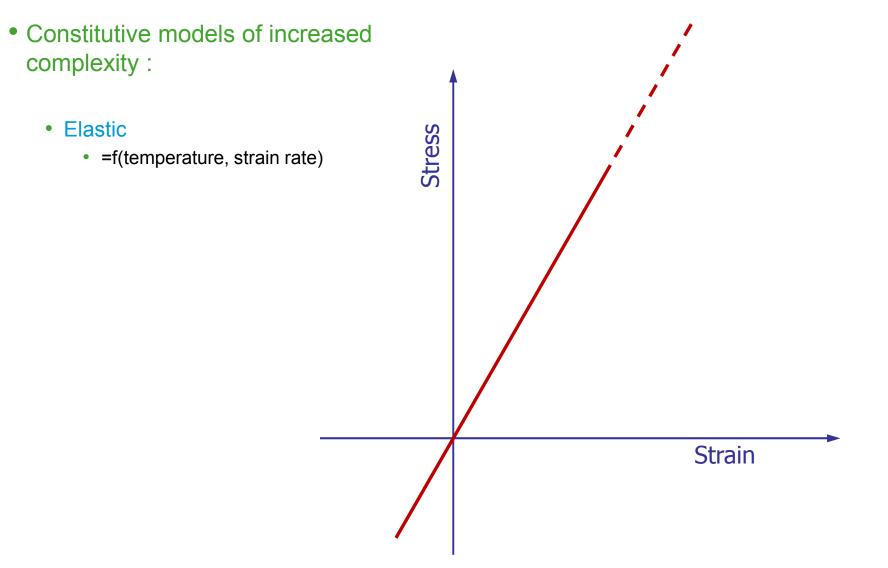
### **MMI ConfidentDesign** Powered by DIGIMAT

The TOOLS, The DATA and The EXPERTIZE that you need to develop optimal polyamide parts.

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- Constitutive models of increased complexity :
  - Stress • Elastic • =f(temperature, strain rate) • Elastoplastic • = f(temperature, strain rate) Strain



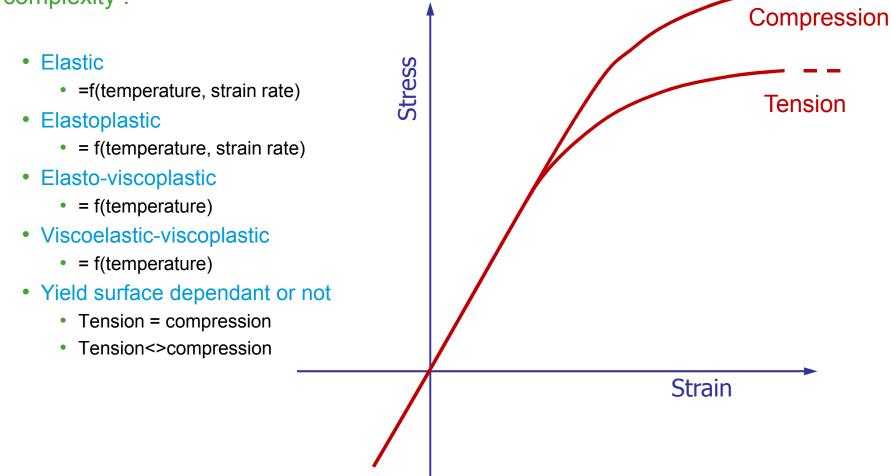
- Constitutive models of increased complexity :
  - $\dot{\varepsilon}_3 > \dot{\varepsilon}_2$  $\boldsymbol{\varepsilon}_3$  $\dot{\varepsilon}_2 > \dot{\varepsilon}_1$ Stress Elastic έ<sub>1</sub> • =f(temperature, strain rate) Elastoplastic • = f(temperature, strain rate) • Elasto-viscoplastic •Same modulus • = f(temperature) Same yield limit **Strain**



- Constitutive models of increased complexity :
  - $\dot{\varepsilon}_2 > \dot{\varepsilon}_1$ Stress Elastic έ<sub>2</sub> • =f(temperature, strain rate) Elastoplastic **έ**<sub>1</sub> • = f(temperature, strain rate) • Elasto-viscoplastic • = f(temperature) **Different Yield Limit**  Viscoelastic-viscoplastic • = f(temperature) **Different Elastic Modulus** Strain

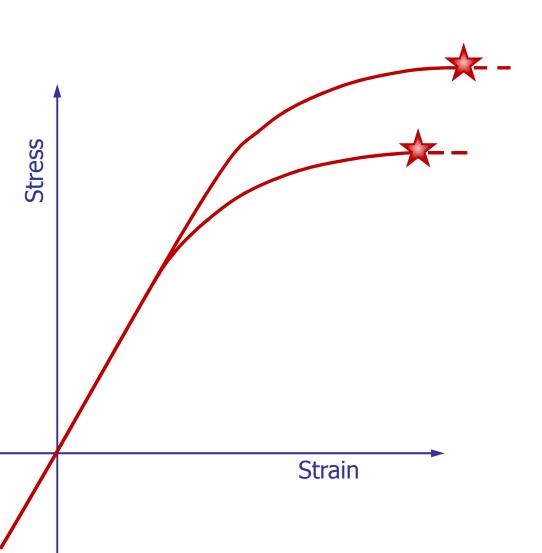


• Constitutive models of increased complexity :





- Constitutive models of increased complexity :
  - Elastic
    - =f(temperature, strain rate)
  - Elastoplastic
    - = f(temperature, strain rate)
  - Elasto-viscoplastic
    - = f(temperature)
  - Viscoelastic-viscoplastic
    - = f(temperature)
  - Yield surface dependant or not
    - Tension = compression
    - Tension<>compression
  - Failure criteria

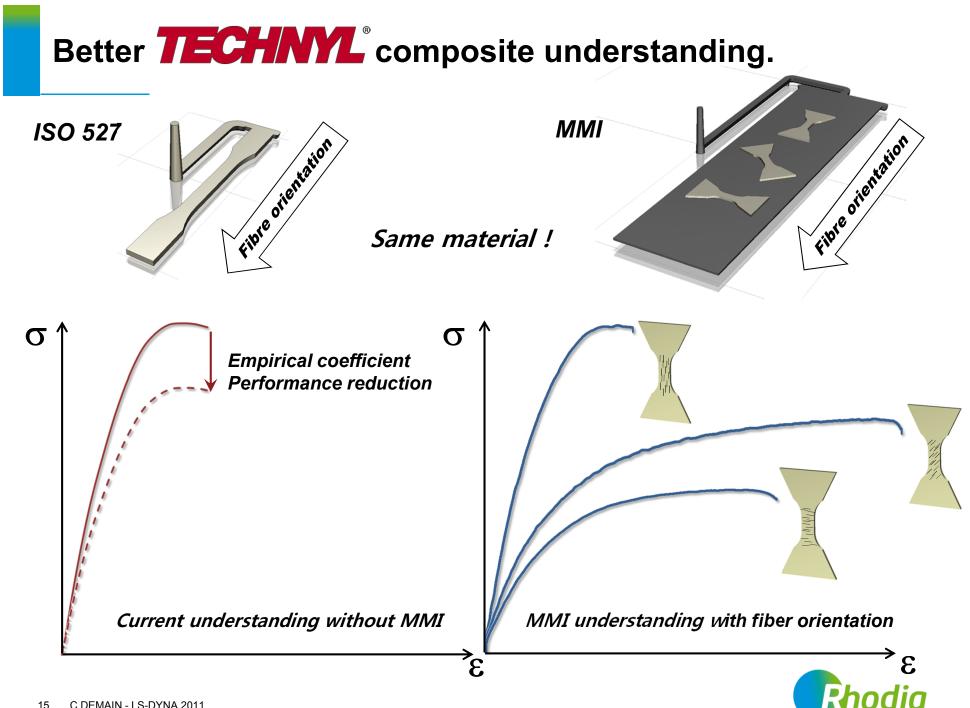


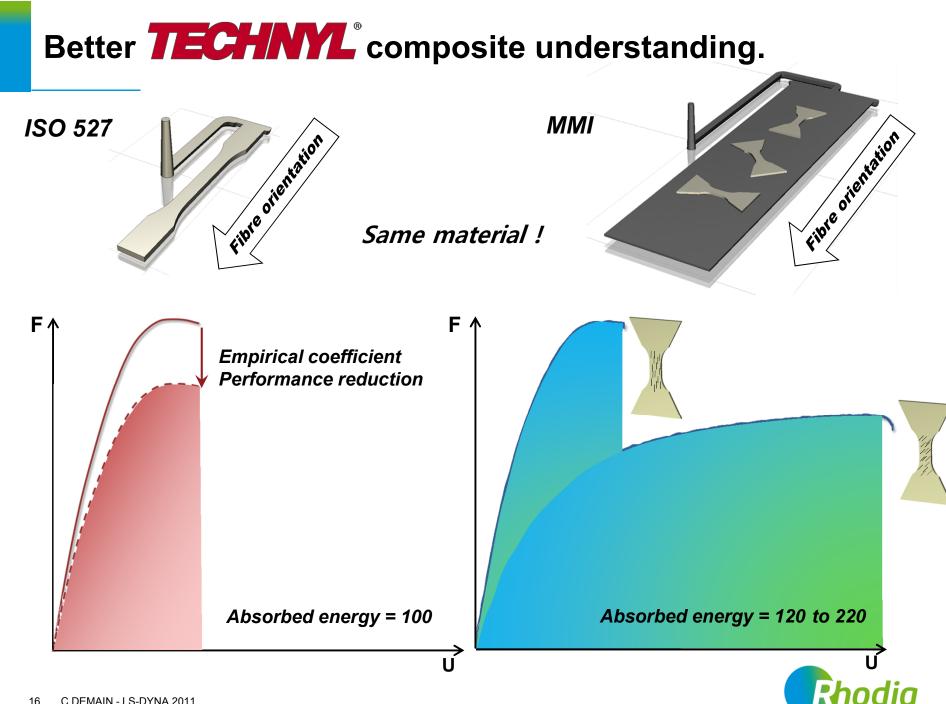


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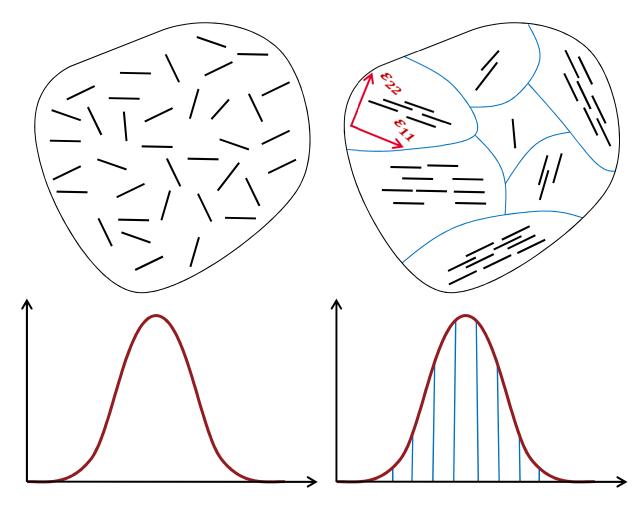






## Better **TECHNYL**<sup>®</sup> composite understanding.

### First Pseudo Grain Failure at integration point



Apply failure indicators on unidirectional composite pseudo grain :

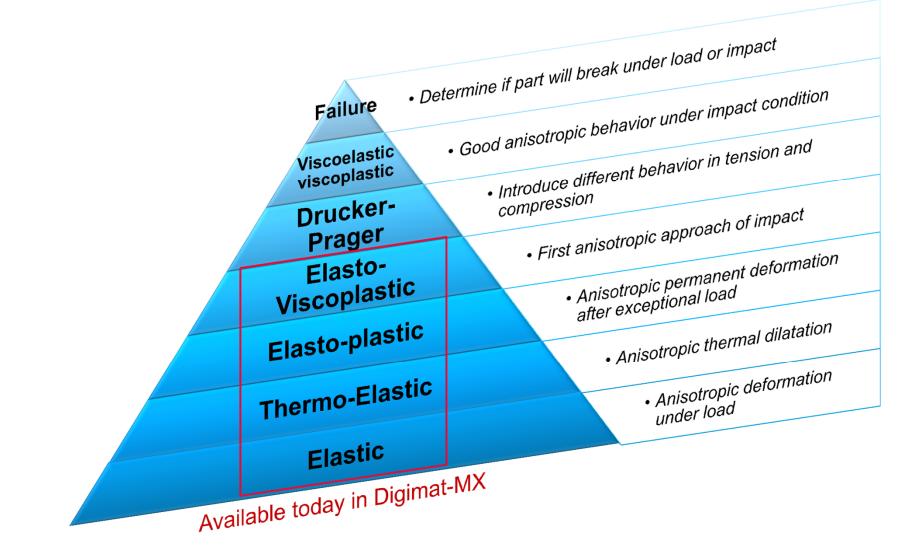
Tsaï Hill 2D strain  $f_A = \frac{\varepsilon_{11}^2}{X_{\varepsilon}^2} - \frac{\varepsilon_{11}\varepsilon_{22}}{X_{\varepsilon}^2} + \frac{\varepsilon_{22}^2}{Y_{\varepsilon}^2} + \frac{4\varepsilon_{12}^2}{S_{\varepsilon}^2}$ 

A micro-structure dependent failure indicator !

A critical number of failed pseudo grain must be defined to activate failure.



## **MMI ConfidentDesign : Data availability**

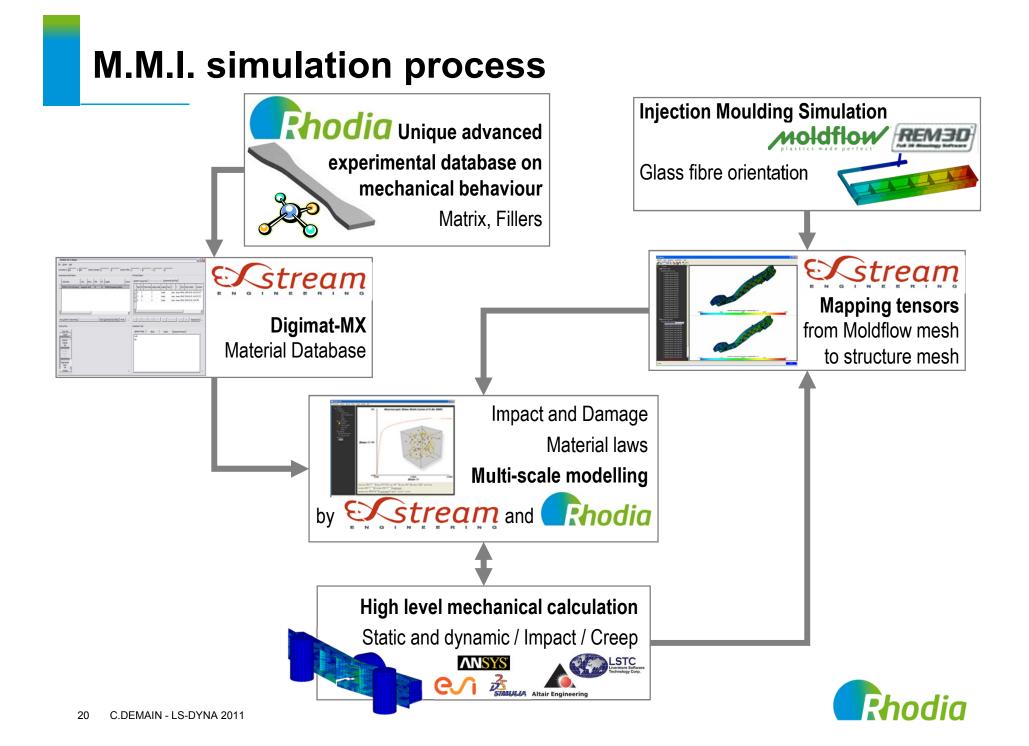




## **MMI ConfidentDesign : Rhodia offer in Digimat-MX**

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				,
Trade Name Type Matrix Filler FA Supplier Comments	DIGIMAT Analysis Files	IGIMAT <u>M</u> aterial	Files Experimental	Data Files
TECHNYL A 218 V35 Black 34 NG Composite PA66 GF 0.35 RHODIA Polyamic Polyamide 66, reinforced with 35% of glass fibre, heat sta TECHNYL A 218G2 V30 Black 34 N Composite PA66 GF 0.3 RHODIA Polyamic Polyamide 66, reinforced with 30% of glass fibre, heat sta	Matrix Model	Temp. RH R	E Date Created	Comments -
TECHNVL A 218G2 V30 Black 34 N Composite PA66 GF 0.3 RHODIA Polyamic Polyamide 66, reinforced with 30% of glass fibre, heat sta TECHNVL A 218G1 V25 Black 34 N Composite PA66 GF 0.25 RHODIA Polyamic Polyamide 66, reinforced with 25% of glass fibre, heat sta	23 elastic	140 50	NO 2010-04-16 14:1	
TECHNYL A 2180 V30 Natural Composite PA66 GF 0.3 RHODIA PolyamicPolyamide 66, reinforced with 30% of glass fibre, heat sta	24 elastic		NO 2010-04-16 14:1	
TECHNYL A 218 V50 Black 21 N Composite PA66 GF 0.5 RHODIA PolyamicPolyamide 66, reinforced with 50% of glass fibre, heat st	25 thermoelastic		NO 2010-04-16 14:1	
TECHNYL A 216 V30 black 21 N Composite PA66 GF 0.2 RHODIA PolyamicPolyamide 66, reinforced with 30% of glass fibre, heat sta	26 thermoelastic		NO 2010-04-16 14:1	5
TECHNYL A 218 V20 Natural Composite PAG6 GF 0.15 RHODIA Polyamic Polyamide 66, reinforced with 15% of glass fibre, heat sta	27 J2 plasticity		NO 2010-04-16 14:1	· ·
TECHNYL A 218 V25 Natural Composite PA66 GF 0.25 RHODIA PolyamicPolyamide 66, reinforced with 25% of glass fibre, heat sta	28 J2_plasticity		NO 2010-04-16 14:1	5
TECHNYL A 218 V30 Natural Composite PA66 GF 0.3 RHODIA PolyamicPolyamide 66, reinforced with 25% of glass fibre, heat sta	29 J2_plasticity		NO 2010-04-16 14:1	
TECHNYL A 218 V35 Natural Composite PAdo GF 0.5 RHODIA PolyamicPolyamide 60, reinforced with 35% of glass fibre, heat statement of the stateme	23     elastic       24     elastic       25     thermoelastic       26     thermoelastic       27     12_plasticity       28     12_plasticity       20     12_plasticity       30     12_plasticity       31     12_plasticity       33     12_plasticity       34     12_plasticity       35     12_plasticity		NO 2010-04-16 14:1	2
TECHNYL A 218 V30 Natural Composite PAG6 GF 0.4 RHODIA Polyamic Polyamice 66, reinforced with 40% of glass fibre, heat sta	31 J2_plasticity		NO 2010-04-16 14:1	
TECHNYL A 218 V50 Natural Composite PA66 GF 0.5 RHODIA PolyamicPolyamide 66, reinforced with 50% of glass fibre, heat sta	32 J2_plasticity		NO 2010-04-16 14:1	5 1 11
TECHNYL A 216 V15 Natural Composite PA66 GF 0.15 RHODIA PolyamicPolyamide 66, reinforced with 15% of glass fibre, for inje	33 J2 plasticity		NO 2010-04-16 14:1	
TECHNYL A 216 V20 Natural Composite PA66 GF 0.2 RHODIA PolyamicPolyamide 66, reinforced with 20% of glass fibre, for inje	34 J2 plasticity		NO 2010-04-16 14:1	
TECHNYL A 216 V30 Black 21 N Composite PA66 GF 0.3 RHODIA PolyamicPolyamide 66, reinforced with 30% of glass fibre, for inje	35 J2_plasticity		NO 2010-04-16 14:1	
TECHNYL A 218 V15 Black 21 N Composite PA66 GF 0.15 RHODIA PolyamicPolyamide 66, reinforced with 15% of glass fibre, heat sta				
TECHNYL A 218 V20 Black 21 N Composite PAG6 GF 0.2 RHODIA Polyamic Polyamide 66, reinforced with 20% of glass fibre, heat sta				<i></i>
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today available in DIGIMAT-MX !	4		0 PA66	Matrix Class





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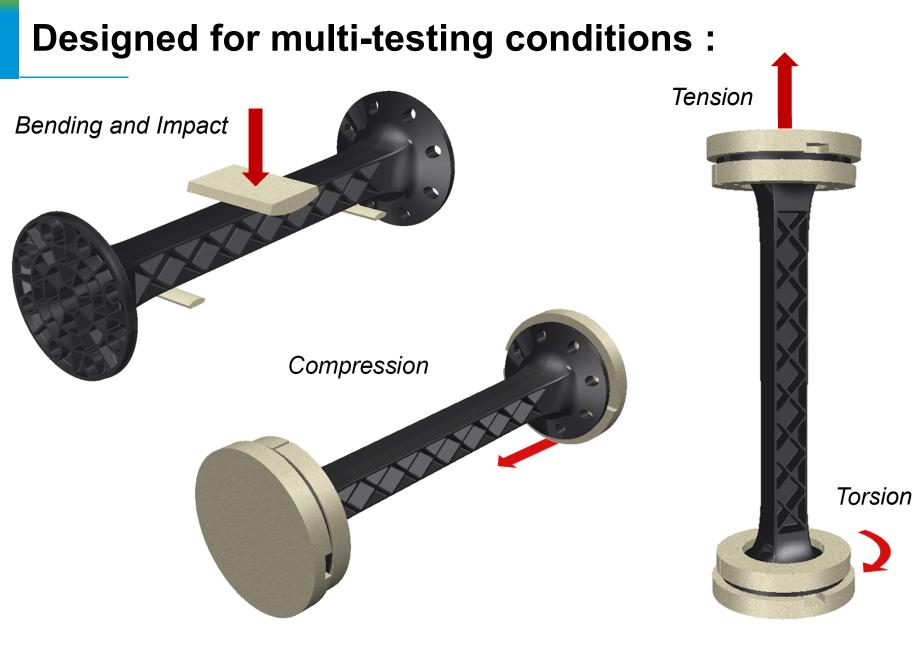


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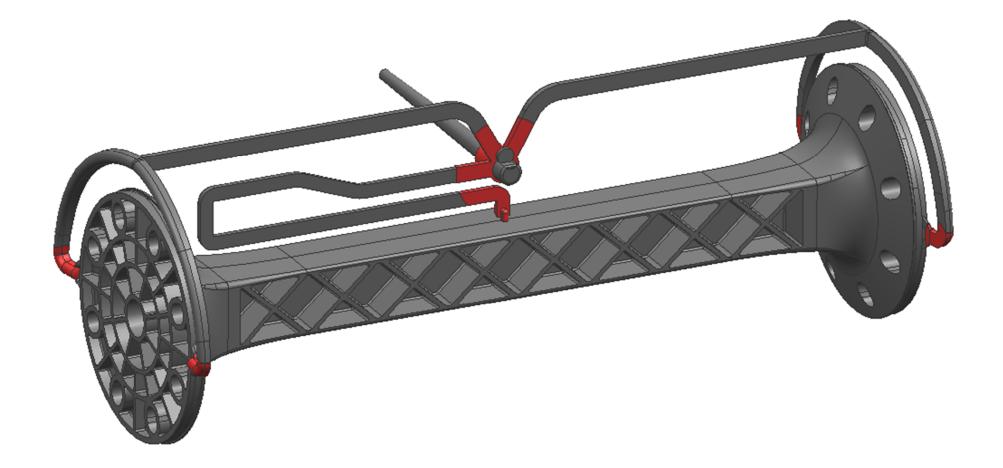
## **The MMI Beam**

#### A new tool to get closer to structural parts



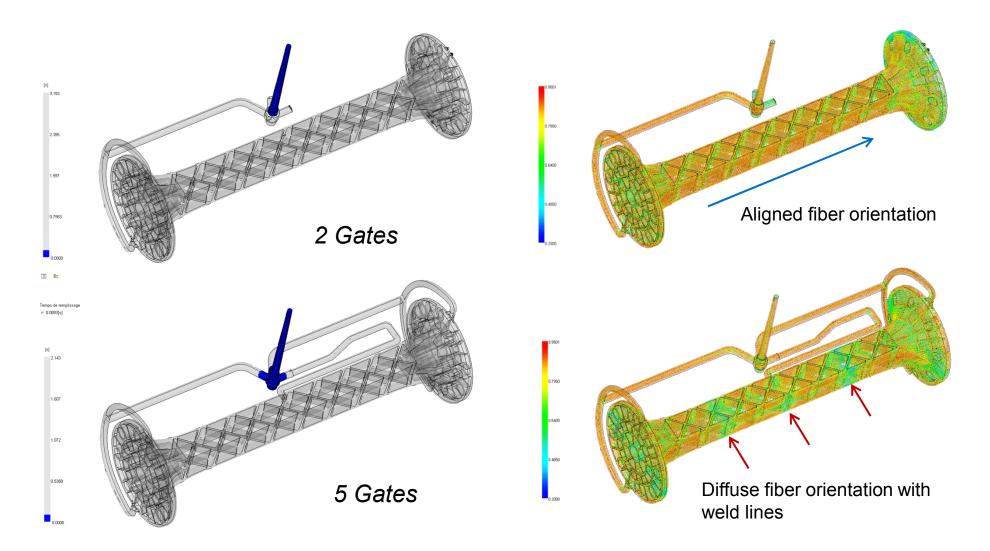


## A multi gating design ...





#### ... to get many different micro-structures







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#### POLYAMIDE Group Lyon Research and Technology Center Digimat to LS-DYNA Simulation

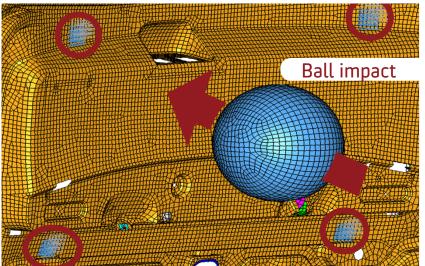
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### Real impact test on a large ribbed part Boundary conditions

Fixations







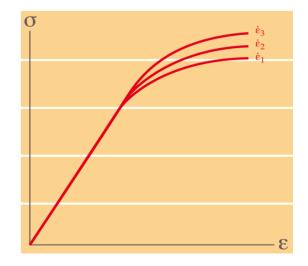
### Real impact test on a large ribbed part Isotropic Material

TECHNYL A218 V30 @ Eh0, 23°C 200 180 160 140 True stress (Mpa) 120 100 80 60 40 Failure plastic strain : 1.8 % 20 0 0.000 0.005 0.015 0.020 0.025 0.010 0.030 0.035 True strain



# Real impact test on a large ribbed part M.M.I Material

- High end use of Digimat software : combining anisotropy and strain rate dependency
  - Glass Fiber :
    - Elastic
    - Aspect Ratio
    - Weight fraction
    - Orientation on all the part
  - PA66 Matrix :
    - Elasto-Viscoplastic
    - Fitted by M.M.I. ConfidentDesign approach
  - Failure criteria :
    - Total strain

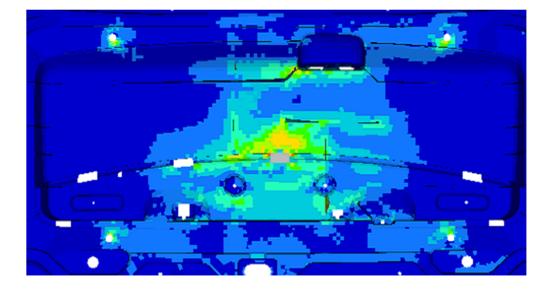




With the courtesy of

### Real impact test on a large ribbed part Isotropic Material





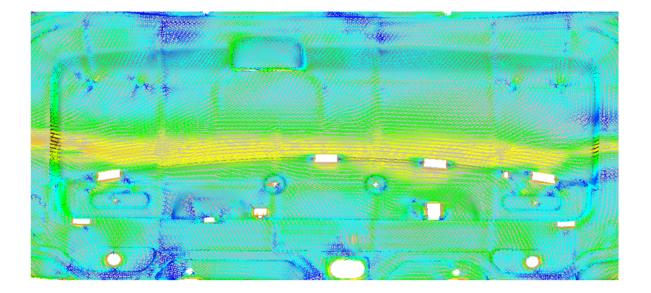
➡ With isotropic material the model do not break

The part fails in real life



# Real impact test on a large ribbed part <u>MMI – injection simulation</u>

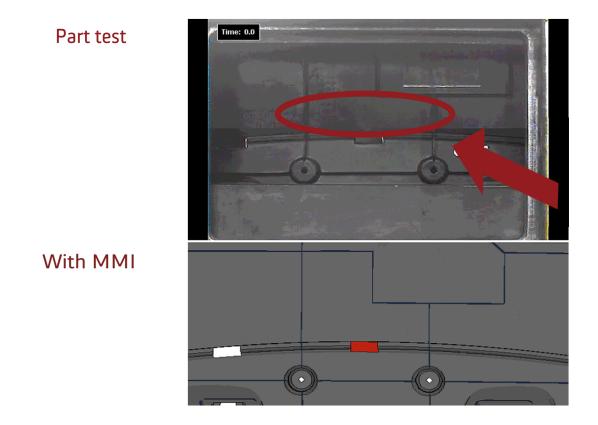
Fiber orientation







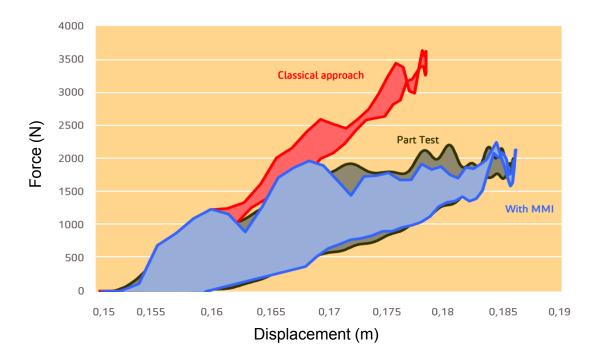
#### Real impact test on a large ribbed part MMI – impact result



Failure area: good correlation achieved with MMI



#### Real impact test on a large ribbed part MMI – energy absorption

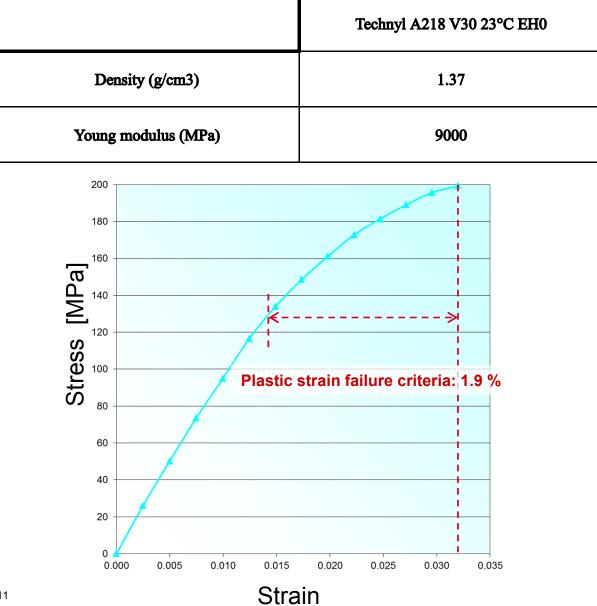




With MMI, excellent energy absorption correlation



## Material isotropic approach



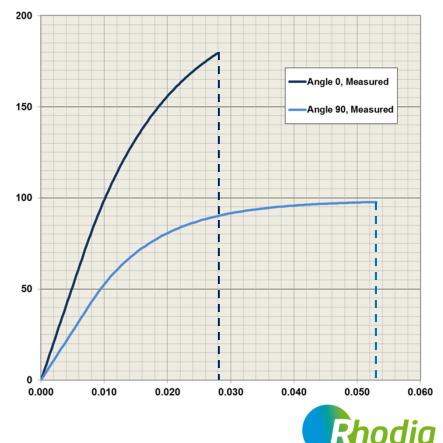


## Material MMI approach

- High end use of Digimat software :
  - Glass Fiber :
    - Elastic
    - Aspect Ratio
    - Weight fraction
    - Orientation on all the part
  - PA66 Matrix :
    - Elasto-Viscoplastic
    - Fitted by M.M.I. ConfidentDesign approach
  - Failure criteria :
    - FPGF (First Pseudo-Grain Failure)
    - Fast determination of FPGF parameters

#### • MMI material definition fitted Elastoviscoplastic with Basic FPGF

Max strain used as FPGF Inputs for Tsaï Hill 2D strain, Critical factor 0.85, no reverse engineering



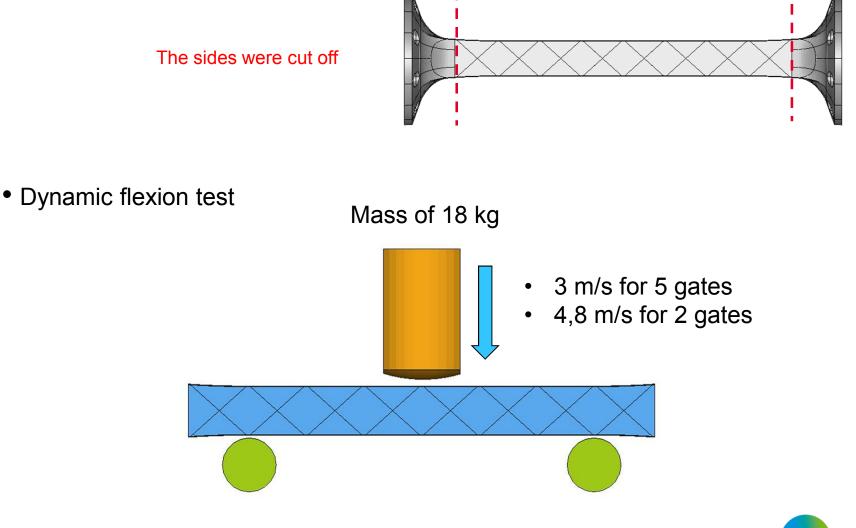
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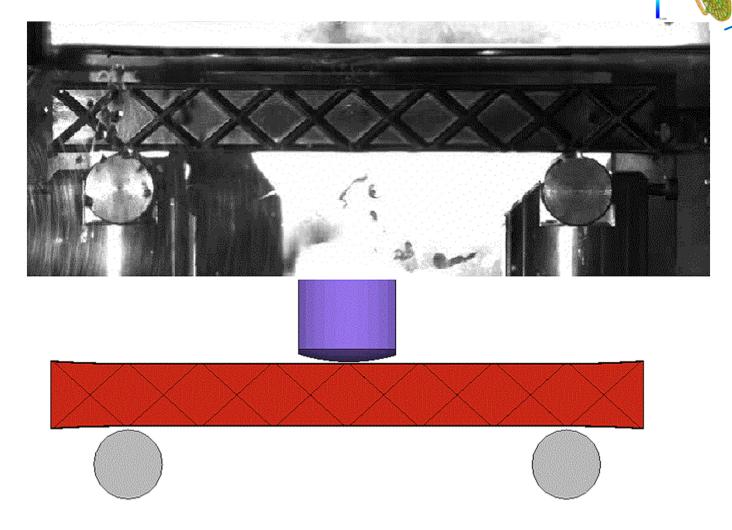


### MMI beam presentation of impact model

• Beam

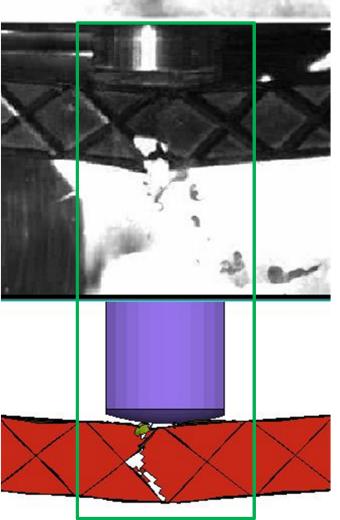


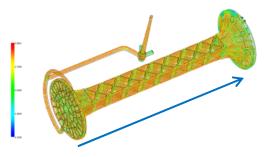
# MMI beam – 2 gates correlation experiment / MMI



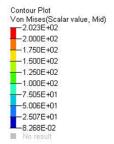


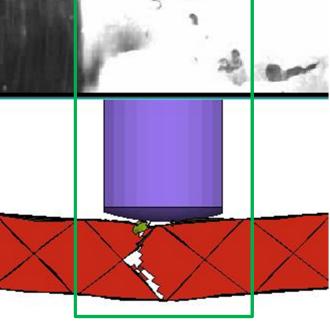
#### MMI beam – 2 gates correlation experiment / MMI





Failure at the same time

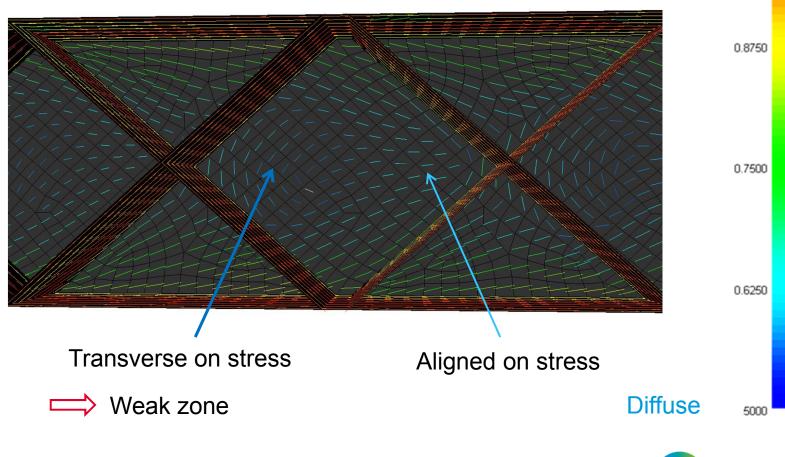






### MMI beam – 2 gates Failure prediction

The failure area could be explained by the fiber orientation

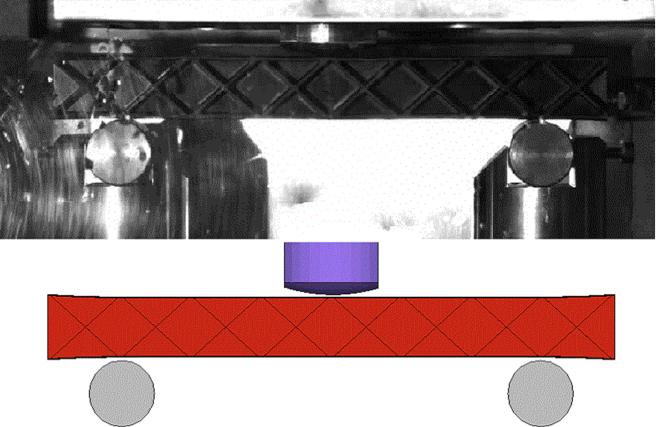


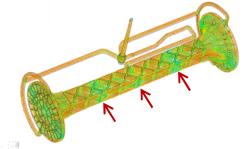


1.000

Aligned

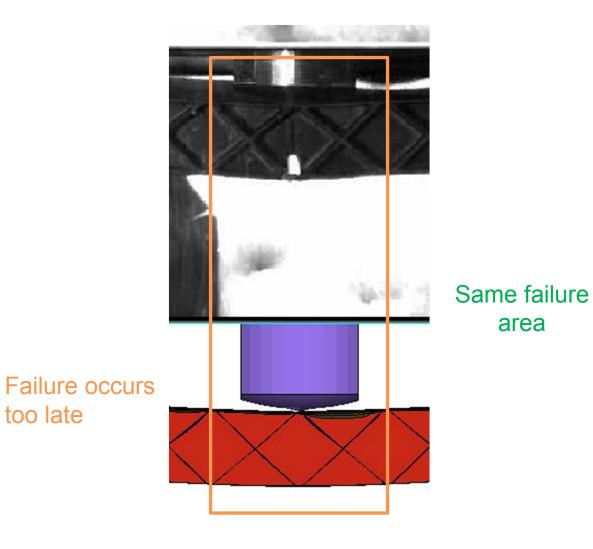
#### MMI beam – 5 gates Failure prediction



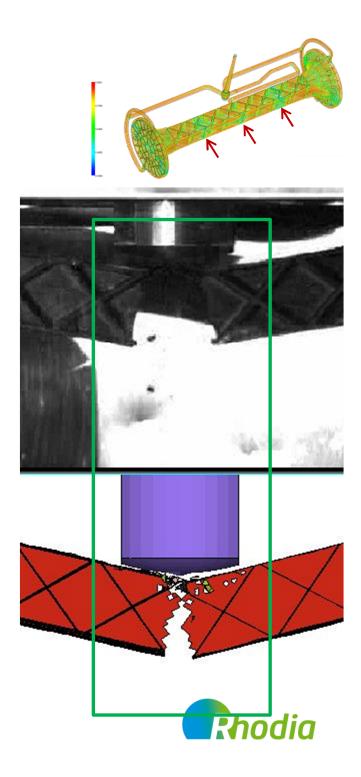




#### MMI beam – 5 gates **Failure** prediction

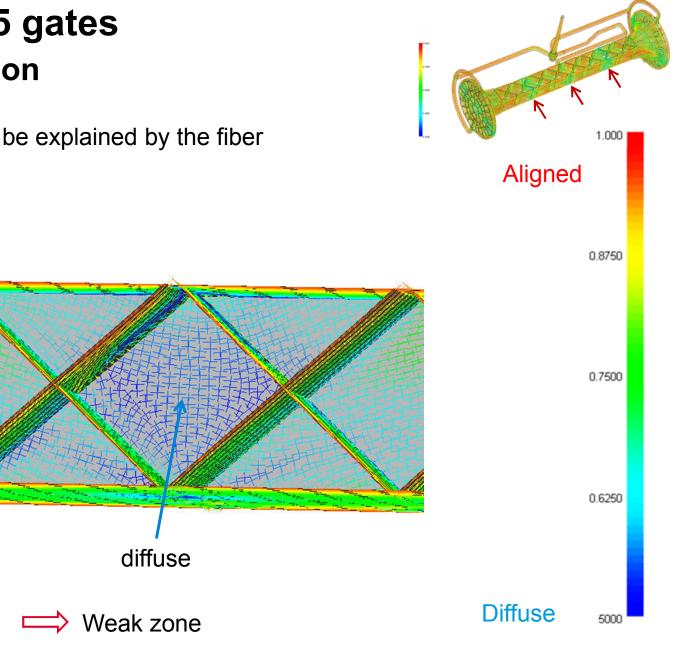


area



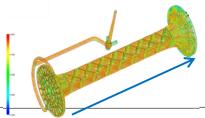
### MMI beam – 5 gates **Failure** prediction

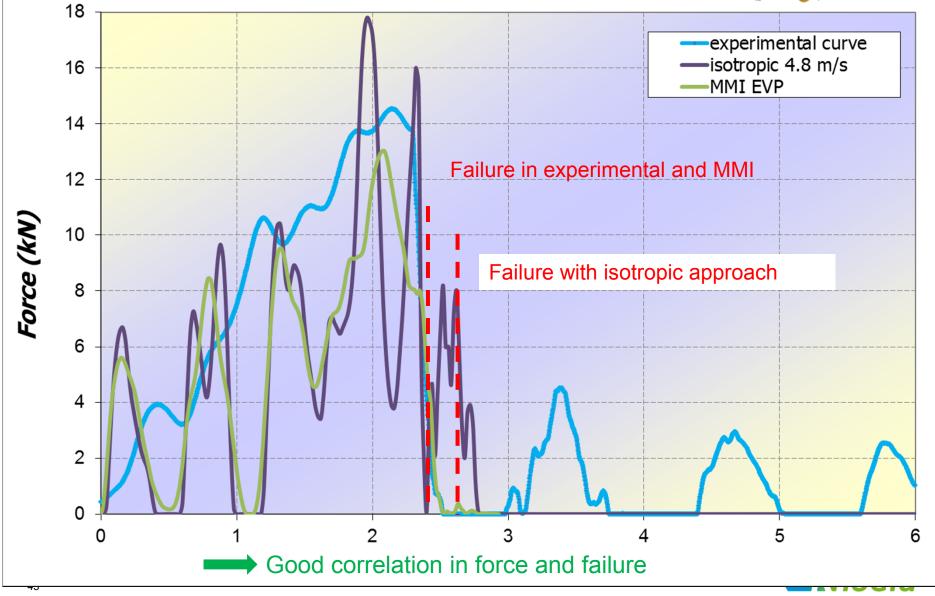
The failure area could be explained by the fiber orientation

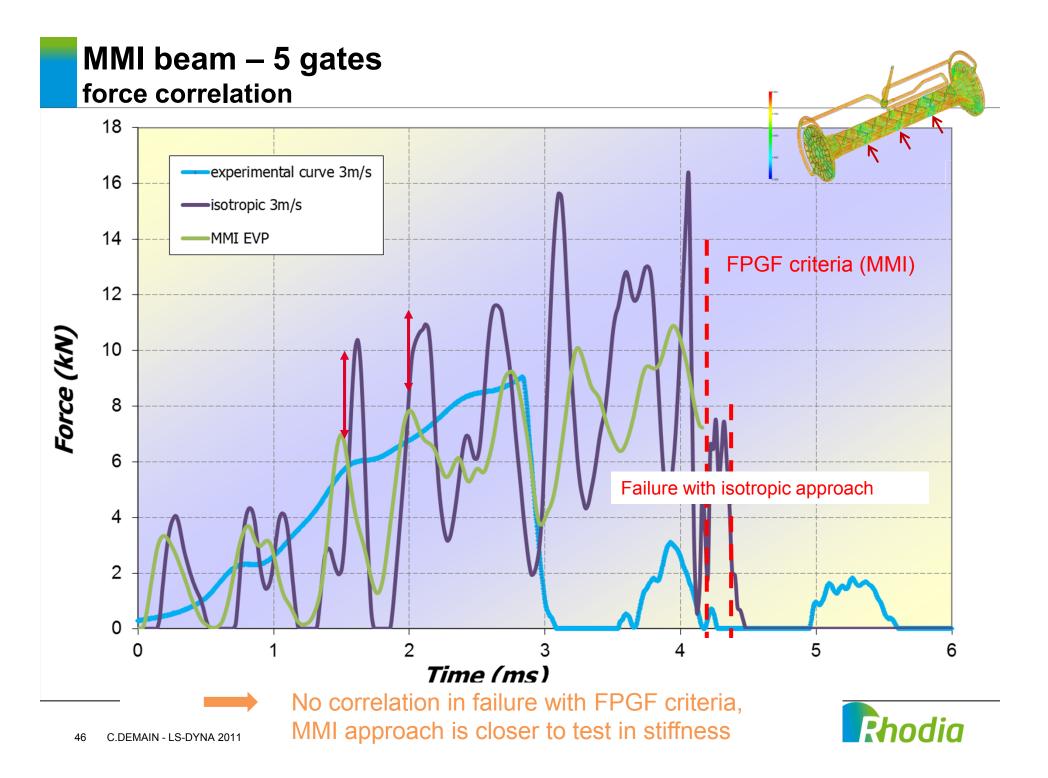




#### MMI beam – 2 gates Force correlation









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## Conclusion

#### Conclusions

#### • With the FPGF failure model

- We obtain some interesting results in 2 gates case :
  - Correlation in term of failure and force
  - Failure related to microstructure
- The failure model is very promising
- To be improved :
  - FPGF parameter
    - Run MMI fitting process on FPGF parameters to get better value on transverse and shear !
  - Material behavior
    - Add hydrostatic pressure dependency (tension/compression behavior)





