Fast Solvers for Large-Scale Systems of Finite Element Equations

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Outline



- 2 Solvers
 - Direct Methods beyond Gaussian Elimination
 - Iterative Methods beyond Jacobi and Gauss-Seidel
 - Domain Decomposition Methods
- 3 Examples and Conclusions
 - Example 1: Source Reconstraction
 - Example 2: Magnetic Valve
 - Conclusions

Where do we need Fast Solvers ?

Implicite time discretization of dynamic problems like

$$\rho \frac{\partial^2 u}{\partial^2 t} + c \frac{\partial u}{\partial t} - \frac{E}{2(1+\nu)} \left(\Delta u + \frac{1}{1-2\nu} \nabla (\nabla \cdot u) \right) = f(x,t)$$
(1)

leads to the solution of large linear systems of FE equations

$$A\underline{u} = \underline{b} \quad \text{in } \mathbb{R}^n$$
 (2)

at each time step, where the system matrix A has the structure

$$\mathbf{A} = \mathbf{M} + \alpha \tau \mathbf{D} + \beta \tau^2 \mathbf{K} \tag{3}$$

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with the time step $\tau = \Delta t$.

Where do we need Fast Solvers ? (cont.)

Similarly, harmonic excitations

$$\hat{f}(x,t) = \hat{f}(x) \exp(i\omega t), \dots$$
(4)

and **static** or **quasistatic** boundary value problems also lead to the solution of large linear systems of FE equations of the form

$$A\underline{u} = \underline{b}$$
 in \mathbb{R}^n

with system matrices of the form (without damping)

$$A = K - \omega^2 M \tag{5}$$

and

$$A = K, \tag{6}$$

respectively.

Direct Methods beyond Gaussian Elimination Iterative Methods beyond Jacobi and Gauss-Seidel Domain Decomposition Methods

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Gaussian Elimination: Ax=b

Gaussian Elimination = *LU* - Decomposition:

$$\begin{pmatrix} u_{11} & u_{12} & u_{13} & \dots & u_{1n} \\ 0 & u_{22} & u_{23} & \dots & u_{2n} \\ 0 & 0 & u_{33} & \dots & u_{3n} \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & u_{nn} \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \\ \vdots \\ x_n \end{pmatrix} = \begin{pmatrix} c_1 \\ c_2 \\ c_3 \\ \vdots \\ c_n \end{pmatrix}.$$

$U\underline{x} = \underline{c} = L^{-1}\underline{b} \implies LU\underline{x} = \underline{b} \implies A = LU$

Complexity Estimate:

- ops $\approx BW^2n = n^{\frac{2d-2}{d}}n = n^{\frac{3d-2}{d}}$
- Memory $\approx BWn = n^{\frac{d-1}{d}}n = n^{\frac{2d-1}{d}}$

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Sparse Direct Methods





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Complexity Estimate:

- Factorization: ops $\approx n^{3/2}$ for d = 2 and n^2 for d = 3
- Solution: ops $\approx n \log(n)$ for d = 2 and $n^{4/3}$ for d = 3

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H-Matrix Technology





• $A \implies \mathcal{A}: ||A - \mathcal{A}|| \le \varepsilon ||A|| \implies \tilde{\mathcal{A}} = \mathcal{LU}$

- $\varepsilon \approx$ = discretisation error \implies Solver !
- $\varepsilon = 10^{-1}...10^{-2} \Longrightarrow$ Preconditioner $C = \mathcal{LU}$!
- Complexity ≈ n up to a polylogarithmical factor !!

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Gauss' Idea for an Iteration



"faß jeden Abend mache ich eine neue Auflage des Cableau, wo immer leicht nachzuhelfen ist. Bei der Einförmigkeit des Meffungsgeschäfts gibt dies immer eine angenehme Unterhaltung; man sicht daran auch immer gleich, od etwas Iweiselhaftes eingeschichen ist, was noch wünschenswert dleidt um. Ich empfehle Ihnen diesen Modus zur Nachahmung. Schwerlich werden die je wieder direct eliminiren, wenigstens nicht, wenn die mehr als zwei Underannte haben. Das indirecte Verschren lächt sich halb im Schlafe ausführen oder man kann während desselden an andere Dinge denten."

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C. F. GAUSS in [2]

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Jacobi and Gauss-Seidel Iterations

Our system of FE equations

$$A\underline{u} = \underline{b} \qquad \iff \qquad \sum_{j=1}^{n} a_{ij}u_j = f_i, \quad i = 1, \cdots, n$$

can be written in the fixed point form as follows

$$u_{i} = -\frac{1}{a_{ii}} \left(\sum_{j=1}^{i-1} a_{ij} u_{j} + \sum_{j=i+1}^{n} a_{ij} u_{j} \right) + \frac{1}{a_{ii}} f_{i}$$

Jacobi:

$$u_i^{k+1} = -rac{1}{a_{ii}} \left(\sum_{j=1}^{i-1} a_{ij} u_j^k + \sum_{j=i+1}^n a_{ij} u_j^k
ight) + rac{1}{a_{ii}} f_i$$

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Gauss-Seidel:

$$u_i^{k+1} = -rac{1}{a_{ii}} \left(\sum_{j=1}^{i-1} a_{ij} u_j^{k+1} + \sum_{j=i+1}^n a_{ij} u_j^k
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Properties of GSI for FE Matrices like A=K

$$u_{i}^{k+1} = -\frac{1}{a_{ii}} \left(\sum_{j=1}^{i-1} a_{ij} u_{j}^{k+1} + \sum_{j=i+1}^{n} a_{ij} u_{j}^{k} \right) + \frac{1}{a_{ii}} f_{i}$$

- Slow convergence, d.h. convergence rate $q = 1 O(h^2)$
- Fast smoothing of $\underline{e}^k = \underline{u} \underline{u}^k$ rsp. $\underline{r}^k = A\underline{e}^k = \underline{b} A\underline{u}^k$



⇒ Combine SMOOTHING with COARSE-GRID-CORRECTION

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Geometrical Multigrid Methods (MGM)



Result: Linear Complexity: ops = $O(n_l \ln(\varepsilon_{+}^{-1})), M = O(n_l)$

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Netgen/NGSolve: Von-Mises Stress in a Crank-shaft



69839 tets, p = 3, 1,105,983 dof, 34 min on 2.4 GHz PC 1.2 GB

Ulrich Langer Fast Solvers

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From Geometric to Algebraic MGM

In Practice, only the fine grid information is usually available:

- the mesh $\tau_h = \tau_l$ and the set $\omega_h = \omega_l$ of nodes,
- the system matrix $A_h = A_l$ and the rhs $\underline{b}_h = \underline{b}_l$.

Then we want to construct the coarse "grid" components from the given fine grid information:

- ω_{j-1} = (ω_j)_C, where ω_j is split into (ω_j)_C and (ω_j)_F on the basis the matrix graph,
- prolongation P_{i-1}^{j} is definded by interpolation.

Once P_{i-1}^{j} is defined, we easily get the

• restriction $R_{j-1}^j = (P_{j-1}^j)^T$,

• coarse grid matrix $A_{j-1} = P_{j-1}^j A_j R_{j-1}^j$, where *j* is runing from *l* to 2.

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AMG: Crank-shaft



171,264 tets, p = 1, 107,625 dof, $\varepsilon = 10^{-8}$, 34 its, 120 sec

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Preconditioned Conjugate Gradient (PCG) Method

PCG:
$$\underline{u}^{new} \leftarrow \underline{u}^{old}$$

{Initialization step}
 $\underline{u} \leftarrow \underline{u}^{old}$...
while $\delta > \varepsilon^2 \delta^0$ do
 $\alpha \leftarrow \delta/(A\underline{s}, \underline{s})$
 $\underline{u} \leftarrow \underline{u} + \alpha \underline{s}$
 $\underline{r} \leftarrow \underline{r} + \alpha A\underline{s}$
 $\underline{w} \leftarrow C^{-1}\underline{r}$
 $\hat{\delta} \leftarrow (\underline{w}, \underline{r})$
 $\beta \leftarrow \hat{\delta}/\delta$
 $\delta \leftarrow \hat{\delta}$
 $\underline{s} \leftarrow \underline{w} + \beta \underline{s}$
end while

Preconditioning step: $\underline{w} = C^{-1}\underline{r}$

- AMG: $\underline{w} = C^{-1}\underline{r} = (I E)A^{-1}\underline{r}$ means the application of 1 V-cycle to $A\underline{w} = \underline{r}$ with the initial guess $\underline{w}^{ini} = 0$.
- $C = \mathcal{LU}$ is a crude ($\epsilon = 10^{-1}$) \mathcal{H} -LU-Factorization of A, i.e. <u>w</u> solves the system $\mathcal{LU}\underline{w} = \underline{r}$.

Result: Linear Complexity Solvers !

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Primal-, DP-, Dual Iterative Substructuring Methods



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Primal Iterative FE Substructuring Methods

$$\begin{pmatrix} K_C & K_{CI} \\ K_{IC} & K_I \end{pmatrix} \begin{pmatrix} \underline{u}_C \\ \underline{u}_I \end{pmatrix} = \begin{pmatrix} \underline{f}_C \\ \underline{f}_I \end{pmatrix} \quad (7) \quad \Leftrightarrow S_C \underline{u}_C = \underline{g}_C \quad (8)$$

- Schur-Complement-PCG: = PCG applied to (8) with the Schur-Complement Preconditioner (SCPC) $C_C \simeq S_C$
- Inexact Solvers: = PCG applied to (7) with the PC

$$C = \begin{pmatrix} I_C & E_{CI} \\ 0 & I_I \end{pmatrix} \begin{pmatrix} C_C & 0 \\ 0 & C_I \end{pmatrix} \begin{pmatrix} I_C & 0 \\ E_{IC} & I_I \end{pmatrix}$$
(9)

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where $C_I \simeq K_I$ and $E_{IC} = E_{CI}^T$ = stable discrete extension !

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Finite Element Tearing and Interconnecting – Overview

Farhat and Roux (1991)

- Domain Decomposition
- Conformal mesh
- Separate d.o.f.
- Continuity → Lagrange multipliers
- Elimination → dual problem
- PCG sub-space iteration

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Finite Element Tearing and Interconnecting – Overview

Farhat and Roux (1991)

Domain Decomposition

- Conformal mesh
- Separate d.o.f.
- Continuity → Lagrange multipliers
- Elimination \rightarrow dual problem
- PCG sub-space iteration



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Interconnecting

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Finite Element Tearing and Interconnecting – Formulas



The unconstraint minimization problem (??) is obviously equivalent to the constraint MP

$$\min_{\underline{\nu}_{C}} \sum_{i=1}^{p} \left(\frac{1}{2} (S_{C,i} \underline{\nu}_{C,i}, \underline{\nu}_{C,i}) - (\underline{g}_{C,i}, \underline{\nu}_{C,i}) \right)$$
(10)

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subject to $\underline{B\underline{v}} = 0$, with $\underline{v} = (\underline{v}_{C,1}, \dots, \underline{v}_{C,p})$. The constraint MP (10) is equivalent to the SPP

$$\begin{pmatrix} S_{C,1} & B_1^\top \\ & \ddots & \vdots \\ & S_{C,\rho} & B_\rho^\top \\ B_1 & \dots & B_\rho & 0 \end{pmatrix} \begin{pmatrix} \underline{u}_{C,1} \\ \vdots \\ \underline{u}_{C,\rho} \\ \underline{\lambda} \end{pmatrix} = \begin{pmatrix} \underline{g}_{C,1} \\ \vdots \\ \underline{g}_{C,\rho} \\ \underline{0} \end{pmatrix} \iff F\underline{\lambda} = \underline{d}.$$

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Finite Element Tearing and Interconnecting – Features

- PCG iteration and preconditioning via local Neumann and Dirichlet solvers
- Allows massive parallelization
- Spectral Condition number cond₂(C⁻¹K) = O((1 + log(H/h))²)
- Robust w.r.t. coefficient jumps

Mandel/Tezaur, 1996 Klawonn/Widlund, 2001 Brenner, 2002

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Finite Element Tearing and Interconnecting – News

New versions:

• Dual-Primal FETI (FETI-DP):

Farhat et al. (2000), Klawonn/Widlund/Dryja (2002),...

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- Balanced Domain Decomposition by Constraints (BDDC): Dohrmann (2003), Mandel/Dohrmann (2003),...
- Inexact Versions (avoid elimination !): FETI: FETI-DP: BDDC: BDDC: Dohrmann (2005)

New Applications:

Structural Mechanics, Contact, Helmholtz, Maxwell etc.

Example 1: Source Reconstraction Example 2: Magnetic Valve Conclusions

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Outline



- 2 Solvers
 - Direct Methods beyond Gaussian Elimination
 - Iterative Methods beyond Jacobi and Gauss-Seidel
 - Domain Decomposition Methods
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Examples and Conclusions

- Example 1: Source Reconstraction
- Example 2: Magnetic Valve
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Medical Source Reconstraction: Problem Describtion

Lead field basis approach to source reconstruction problems developed by Grasedyck, Hackbusch and Wolters (MPI Leipzig):



5 layer head model Triangulation is given, n = 147287



conductivity $\sigma : \Omega \to \mathbb{R}^{3 \times 3}$ is given

Medical Source Reconstraction: Model and Results

Submodel in the SRP: Neumann BVP

 $-\operatorname{div}(\sigma\nabla u) = f \text{ in } \Omega \subset \mathbb{R}^3 \text{ and } \partial_n u = 0 \text{ on } \partial\Omega$ (11)

- Finite Element discretisation $\rightsquigarrow Ax = b$
- The system has to be solved for $\approx r = 400$ right-hand sides
- Stopping criterion: $||Ax b|| \le 10^{-8} ||b||$
- Machine: SUNFire, 900 MHz, single processor

| | Pardiso | $\mathcal{H}	ext{-}LU(arepsilon=10^{-6})$ | PEBBLES |
|-------|---------|---|---------|
| Setup | 237 | 468 | 13 |
| Solve | 2.4 | 1.0 | 10 |
| Total | 1197 | 868 | 4013 |

Pardiso (Gärtner/Schenk) *H*-LU (Grasedyck/LeBorne/Kriemann) PEBBLES (Langer/Haase/Reitzinger) multiple rhs optimisation multiple rhs optimisation multiple rhs optimisation

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Magnetic Valve: Model and FE Model



Joint work with M. Kaltenbacher, R. Lerch, M. Schinnerl and J. Schöberl !

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LAMÉ-NAVIER coupled with MAXWELL

• LAMÉ-NAVIER's Equations + BC + IC:

$$\rho \frac{\partial^2 d}{\partial^2 t} + c \frac{\partial d}{\partial t} - \frac{E}{2(1+\nu)} \left(\Delta d + \frac{1}{1-2\nu} \nabla (\nabla \cdot d) \right) = f_V(A)$$

• MAXWELL's Equations + BC + IC:

$$\sigma \frac{\partial A}{\partial t} + \operatorname{curl}(\frac{1}{\mu(|\operatorname{curl}(A)|)}\operatorname{curl}(A)) + \sigma \frac{\partial d}{\partial t} \times \operatorname{curl}(A) = S$$

- Coupling terms:
 - LAMÉ: (volume) Lorentz-forces + (surface) interface forces

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MAXWELL: electromotive force + Ω_{mag} = Ω_{mag}(d)

Example 1: Source Reconstraction Example 2: Magnetic Valve Conclusions

Implicite Time Integration of the FE Equations

Mechanical nodal FE Mesh

- 1. Mechanical Predictor $\tilde{d} = d_n + \Delta t v_n + 0.5 \Delta t^2 (1 - 2\beta) a_n$ $\tilde{v} = v_n + (1 - \gamma) \Delta t a_n$
- 5. Mechanical Solver Multi-Grid-Solver:

 $M^*a_{n+1} = f_{n+1}^*$

with $M^* = M + \gamma \Delta t C + \beta \Delta t^2 K$ $f^*_{n+1} = f_{n+1} - K \tilde{d} - C \tilde{v}$ Corrector: $d_{n+1} = \tilde{d} + \beta \Delta t^2 a_{n+1}$ $v_{n+1} = \tilde{v} + \gamma \Delta t a_{n+1}$

6. Convergence Test

Magnetic edge FE Mesh

- 2. Update the magnetic quantities
- 3. Magnetic Solver Predictor: $\tilde{A} = A_n + (1 - \alpha)\Delta tR_n$ Multi-Grid-Solver:

 $L^*R_{n+1}=Q_{n+1}^*$

with $L^* = L + \alpha \Delta t P$ $Q_{n+1}^* = Q_{n+1} - P \tilde{A}$ Corrector: $A_{n+1} = \tilde{A} + \alpha \Delta t R_{n+1}$

4. Calculate the induction and the magnetic forces

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Example 1: Source Reconstraction Example 2: Magnetic Valve Conclusions

Simulation Results

Simulation vs Measurments

Parallel Processing



| P | 1 | 4 | 16 | 16 |
|-------|-----|-----|------|------|
| m | 2 | 2 | 2 | 30 |
| [sec] | 453 | 99 | 31 | 458 |
| Sp | 1.0 | 4.6 | 14.5 | 0,93 |

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 \Rightarrow Valve Movie

⇒ Cave Movie

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- Sparse Direct Methods
- Fast Iterative Methods
- Preconditioners and Krylow-Space-Iterations
- DDM as Parallelization Technology

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Summary II

Efficient solvers are hybrid methods which exploit the best properties of both worlds, the world of direct and itereative methods:

- *H*-matrix techniques:
 - From Solver to Preconditioner:
 - \mathcal{H} -LU($\varepsilon = 10^{-6}$) to C= \mathcal{H} -LU($\varepsilon = 10^{-1}$)
- Algebraic Multigrid
 - iterative methods as smoothers combined with
 - sparse direct solvers for the systems on the coarsest grid
- Domain Decomposition Methods
 - sparse direct solvers on the subdomains combined with

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iterative solvers for the interface problems

Thanks to

- Dr. K. Gärtner (WIAS, Berlin) for PARDISO
- Prof.Dr. W. Hackbusch and his colleagues (MPI, Leipzig) for *H*-matrix-results and the hlib
- Prof.Dr. J. Schöberl (RWTH Aachen, RICAM Linz) for NGSolve results
- my colleagues and my former colleagues from Linz

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References

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- *H*-Matrix-Software: www.hlib.org
- NGSolve: www.femworks.at
- PEBBLES: www.numa.uni-linz.ac.at /Research/Projects/pebbles.html
- Multigrid Methods: www.mgnet.org
- AMG (Stüben):

www.scai.fraunhofer.de/samg.html

- Boomer-AMG:www.llnl.gov/CASC
- Domain Decomposition Methods: www.ddm.org

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