





Dreidimensionale, Kontinuumsmechanische Modellierung des Muskuloskeletalen Apparates





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Motivation

- Different skeletal muscle modelling approaches
- Overview on forward-dynamics and inverse-dynamics musculoskeletal modelling approaches
- Short comings
- Modelling framework of a two-muscle model upper limb model

OVERVIEW

- Geometrical Model
- Continuum-mechanical skeletal muscle model
- Solving the musculoskeletal system
- Simulation results
 - Convergence studies
 - Contact forces acting within the system
- Outlook

Motivation

Modelling

Simulation







Basic Principles of Forward / Inverse Dynamics

Forward / inverse dynamics musculoskeletal modelling

Forward dynamics

Optimisation of cost

length targets

Control mechanisms / EMG

(experimental data driven)

functions associated with

the control or muscle

Motivation

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Simulation

Outlook

Muscle Force

Joint Load

Motion

Movement

Muscle recruitment

Inverse dynamics

- Cost functions
- Muscle grouping
- Experimental Data (EMG) / assumptions on muscle activities

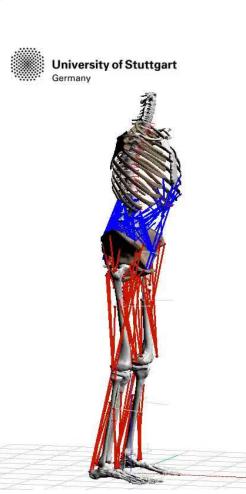






THE MUSCULOSKELETAL SYSTEM

- There exist many different approaches to model the mechanical behavior of skeletal muscle:
 - Biophysical Huxley-type models (including the neuromuscular system)
 - (Chemo-)Electro-mechanical skeletal muscle models
 - Continuum-mechanical skeletal muscle models
 - Hill-type skeletal muscle models
- Modelling the musculoskeletal system:
 - Inverse dynamics models
 - Forward dynamics models
- State-of-the-art musculoskeletal system models:
 - Inverse dynamics models using Hill-type skeletal muscle models



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Forward dynamics simulations courtesy of JP Syn Schmitt, Institut für Sport- und Bewegungswissenschaft, Universität Stuttgart







- Limitations of the state-of-the-art models:
 - Hill-type skeletal muscle models are lumped-parameter discrete models that have difficulties to take into account any spatial characteristics of skeletal muscles.

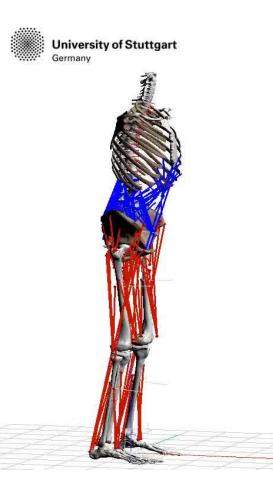
LIMITATIONS OF EXISTING MUSCULOSKELETAL MODELS

 They cannot take into account any contact between skeletal muscles and surrounding structures.



Three-dimensional, continuummechanical skeletal muscle models

- Challenges of continuum-mechanical models:
 - Continuum-mechanical models of musculoskeletal systems are rare:
 - → Only a few inverse-dynamics approaches exist
 - → Forward-dynamics frameworks do not exist
 - Computational expensive
 - Convergence due to the force-length relationship



Motivation

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THE UPPER LIMB MODEL

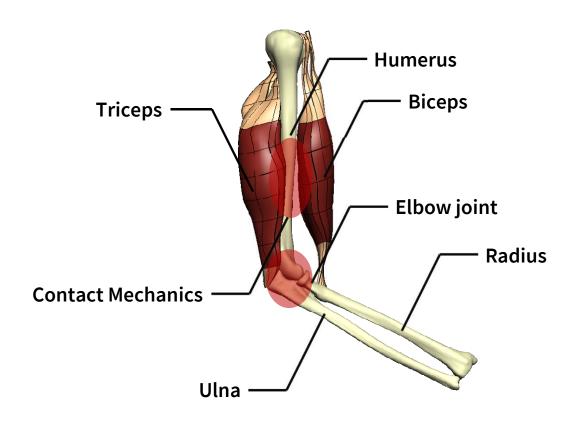
Model components from Visible Human Project

Modelling

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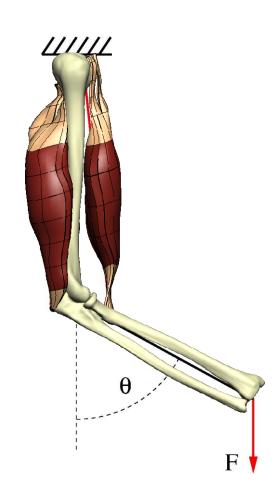


Motivation

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THE UPPER LIMB MODEL

Introducing the equivalent static system

- Muscle length is modelled as the distance between muscle origin and insertion
- Formulating the momentum balance in the elbow joint:

$$T(\theta, \alpha_T) l_T(\theta) + F l_F(\theta) - B(\theta, \alpha_B) l_B(\theta) = 0$$

- Initially, the lever arms are be determined using the tendon displacement method or using the actual geometry of the system
- Muscle forces are determined by FEM simulations using the continuum mechanical muscle approach







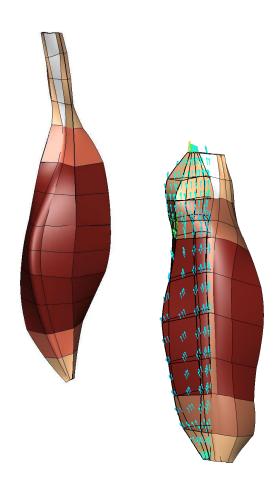
CONTINUUM-MECHNICAL CONSTITUTIVE EQUATIONS

Motivation

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- Continuum-mechanical models describe the mechanics of the muscle and surrounding tissue.
- Assumptions on skeletal muscles model:
 - Hyperelastic, incompressible, transversely isotropic
 - Stress-strain relation (constitutive equation)

$$\mathbf{S}_{\mathrm{MTC}} = \mathbf{S}_{\mathrm{iso}} + \mathbf{S}_{\mathrm{aniso}} = \mathbf{S}_{\mathrm{iso}} + (\mathbf{S}_{\mathrm{passive}} + \alpha \, \gamma_{\mathrm{M}} \, \mathbf{S}_{\mathrm{active}}) \, (1 - \gamma_{\mathrm{ST}})$$

tissue	contribution	parameter	triceps	biceps	source
muscle	isotropic	$c_{1M} \ c_{2M}$	$3.56 \cdot 10^{-2} \text{ MPa}$ $3.86 \cdot 10^{-3} \text{ MPa}$	$3.56 \cdot 10^{-2} \text{ MPa}$ $3.86 \cdot 10^{-3} \text{ MPa}$	[HaBe1994]
	passive	$rac{c_{3M}}{c_{4M}}$	$4.02 \cdot 10^{-7} \text{ MPa}$ 38.5 [-]	$3.57 \cdot 10^{-8} \text{ MPa}$ 42.6 [-]	[Zhen1999]
	active	$\Delta W_{ m asc}$ $\Delta W_{ m desc}$ $ u_{ m asc}$ $ u_{ m desc}$ $ u_{ m opt}$ $ u_{ m f}$ $ u_{ m max}$	0.30 [-] 0.10 [-] 4.00 [-] 4.00 [-] 1.3 [-] 0.30 MPa	0.25 [-] 0.15 [-] 3.00 [-] 4.00 [-] 1.35 [-] 0.30 MPa	adapted from [Gunt2007]
tendon ·	isotropic	$egin{array}{c} c_{1T} \ c_{2T} \end{array}$	$\begin{array}{c} 2.31 \mathrm{MPa} \\ 1.15 \cdot 10^{-6} \mathrm{MPa} \end{array}$	2.31 MPa $1.15 \cdot 10^{-6} \text{ MPa}$	WeGa2001]
	passive	c_{3T} c_{4T}	7.99 MPa 16.6 [-]	7.99 MPa 16.6 [-]	[WeGa2001]

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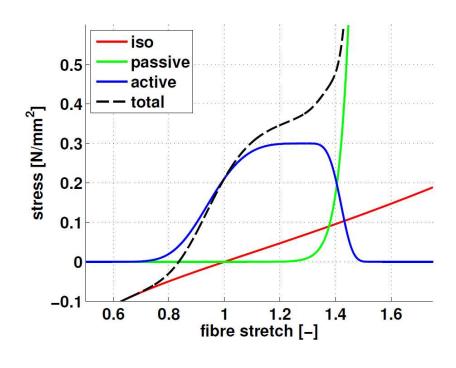
CONTINUUM-MECHNICAL CONSTITUTIVE LAW

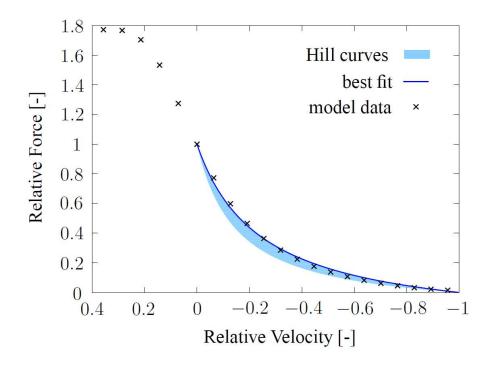
Motivation

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Force-length relationship

Force-velocity relationship







SOLVING THE EQUILIBRIUM EQUATIONS

Challenge: Solve the equilibrium equations using the muscle forces stemming from the 3D, continuum-mechanical tissue models:

$$T(\theta, \alpha_T) l_T(\theta) + F l_F(\theta) - B(\theta, \alpha_B) l_B(\theta) = 0$$

Position-driven scenario (activation for a particular elbow position / "inverse model")

$$\alpha_T^{(i+1)} = \alpha_T^{(i)} - \frac{M^{(i)}}{\frac{\partial M^{(i)}}{\partial \alpha_T}}, \quad \text{i=1,...,n} \;, \quad \text{with} \qquad \frac{\partial M^{(i)}}{\partial \alpha_T} \approx \frac{\Delta M^{(i)}}{\Delta \alpha_T^{(i)}} = \frac{M^{(i)} - M^{(i-1)}}{\alpha_T^{(i)} - \alpha_T^{(i-1)}} = \frac{T^{(i)} - T^{(i-1)}}{\alpha_T^{(i)} - \alpha_T^{(i-1)}}$$

Activation-driven scenario (elbow angle for a prescribed activation / "forward model"):

$$\theta^{(i+1)} = \theta^{(i)} - \frac{M^{(i)}}{\frac{\partial M^{(i)}}{\partial \theta}}, \quad \text{i=1,...n} \,, \quad \text{with} \qquad \frac{\partial M^{(i)}}{\partial \theta} \approx \frac{\Delta M^{(i)}}{\Delta \theta^{(i)}} = \frac{M^{(i)} - M^{(i-1)}}{\theta^{(i)} - \theta^{(i-1)}}$$

Force-driven scenario can be described in a similar way.

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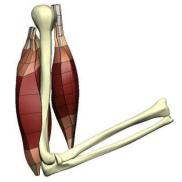
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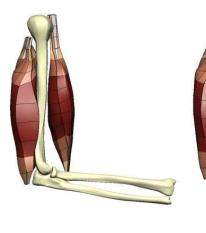


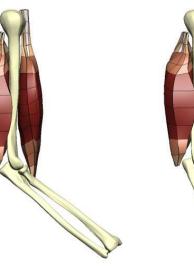




SKELETAL MUSCLES AS ISOLATED SIMULATIONS







Motivation

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Simulation

Outlook

- Investigating for the full range of motion, i.e.,
 - Motion $[10 \le \theta \le 150]$, activation $[0 \le \alpha \le 1]$, with/ without contact
- The impact on:
 - Reaction forces' magnitude and orientation
 - Fibre stretch and resulting muscle shapes
 - Impact of muscle-bone interaction

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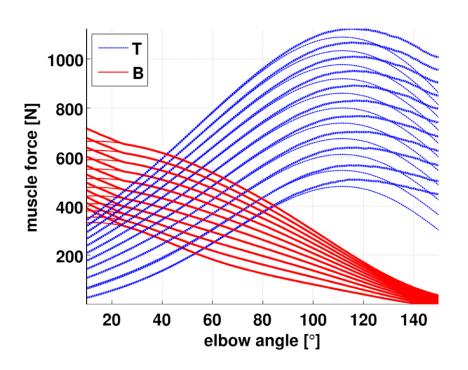
Muscle and Contact Forces

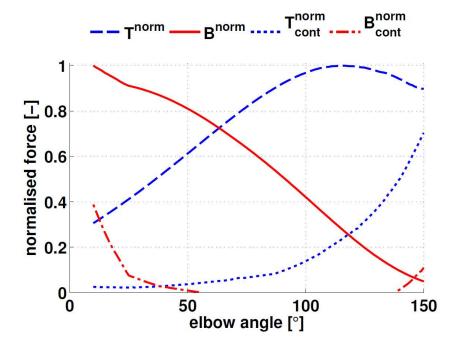
 Muscle forces for the full range of motion and different levels of activation (left) and the contact reaction forces (right) for full activation of the biceps and the triceps muscle.



Modelling

Simulation









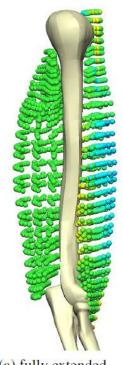


IMPACT OF CONTACT ON MUSCLE FIBRE DISTRIBUTION

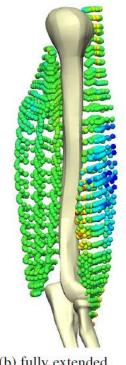
Motivation

Modelling

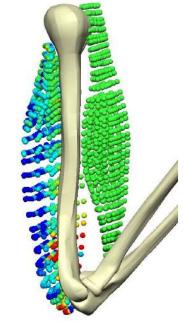
Simulation



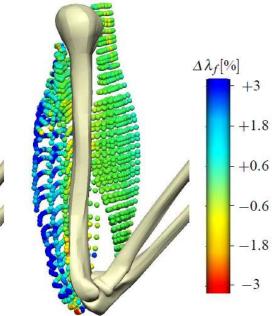
(a) fully extended, $\theta = 10^{\circ}$, and $\alpha = 0$



(b) fully extended, $\theta = 10^{\circ}$, and $\alpha = 1$



(c) fully flexed, $\theta = 150^{\circ}$, and $\alpha = 0$



(d) fully flexed, $\theta = 150^{\circ}$, and $\alpha = 1$







POSITION-DRIVEN SCENARIO

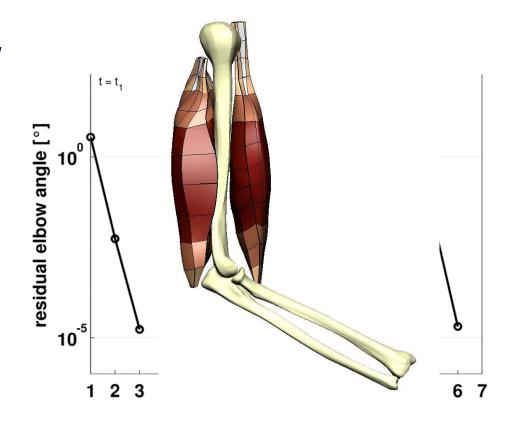
 By assuming variations in activation, one can achieve "forward dynamics" simulation, hence

• with
$$\bar{\alpha}_T = 0.09$$
, $\bar{F} = 44$ N and $\alpha_B(t_1) = 88.58\% \rightarrow \theta_{equi} = 57.47^\circ$ $\alpha_B(t_2) = 32\% \rightarrow \theta_{equi} = 38.27^\circ$ $\alpha_B(t_3) = 65\% \rightarrow \theta_{equi} = 50.10^\circ$



Modelling

Simulation







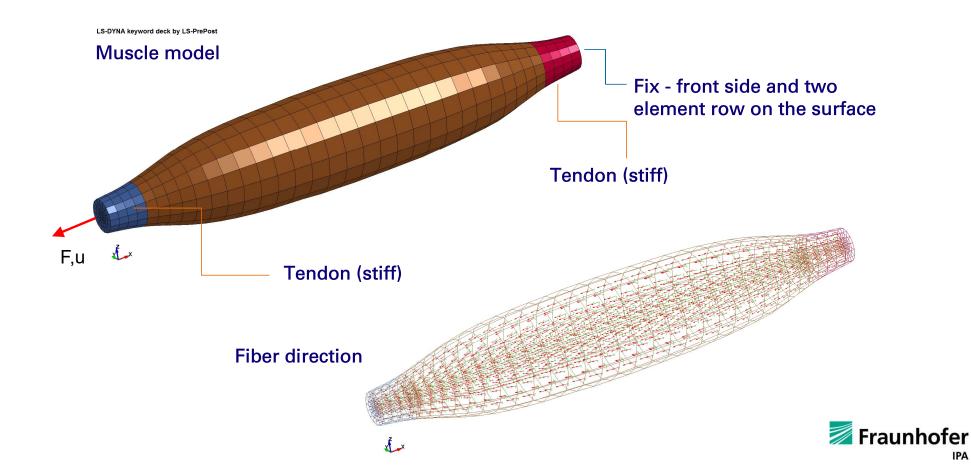


USER MATERIAL IMPLEMENTATION IN LS-DYNA

Motivation

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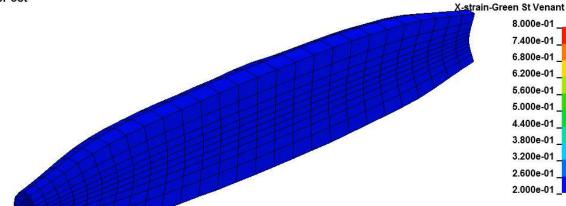




A DISPLACEMENT-DRIVEN SCENARIO

LS-DYNA keyword deck by LS-PrePost Time = 0

Contours of X-strain-Green St Venant min=-6.19888e-06, at elem# 4405 max=5.72205e-06, at elem# 3670



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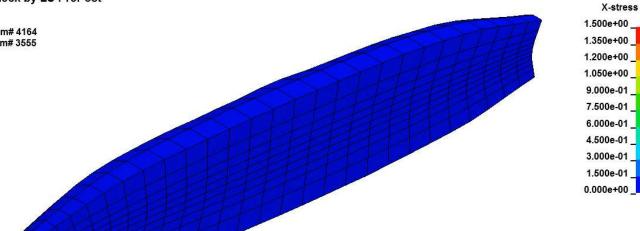




A FORCE-DRIVEN SCENARIO

LS-DYNA keyword deck by LS-PrePost Time = 0

Contours of X-stress min=-3.24914e-07, at elem# 4164 max=1.13872e-06, at elem# 3555



Motivation

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FULL UPPER ARM MODEL

- Implicit dynamic simulation of an upper arm motion
 - The muscle, muscle-tendon and tendon behavior are modelled with the proposed constitutive law
 - All bones are assumed to be rigid
 - The biceps is assumed to be fusiform.
 - The triceps us assumed to be bipennate.
 - Both muscles are fully activated within the first second of the motion

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Motivation

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VALIDATION - HIGH DENSITY EMG

- Part of the Fraunhofer MAVO EMMA-CC we aim to
 - Look at research questions arising in ergonomics
 - Use HD-EMG data to determine muscular activation
 - Use Motion Capture analysis techniques to determine movement





Motivation

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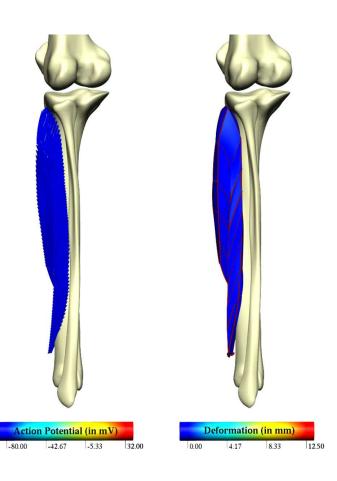
DETAILED CHEMO-ELECTRO-MECHANICAL MODELS

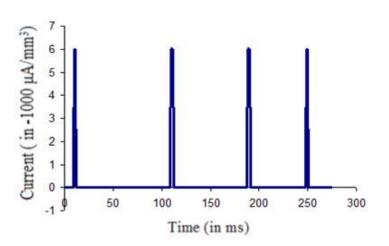
Motivation

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Stimulation protocol defining $I_{\text{stim}}(t)$ at the nodal locations of the neuromuscular junctions.

O. Röhrle, "Simulating the Electro-Mechanical Behavior of Skeletal Muscles", IEEE Computing in Science and Engineering, DOI 10.1109/MCSE.2010.30







Extension to a multiple muscle scenario

- Contact between multiple muscles
- Control strategies for multiple muscles? Solving the forward problem
- Extension to chemo-electro-mechanical skeletal muscle models and biophysical based neuromuscular models for muscle recruitment

OUTLOOK

- Couple continuum-mechanical models with Hill-type modelling approaches like the forward-Inverse-dynamics model (Bezier, Lloyd,...) to drive the model (predictor-corrector)
- Model order reduction for muscles

Moment arm calculation

 Currently, the common (analytical) method of An (1992) is used. However, due to the knowledge of the muscle force directions and the resulting geometry, accurate moment arms can be computed

Validation

- Biodex experiments for moment arms
- Linking experimentally determined EMG data to drive the model and validate motion.

Motivation

Modelling

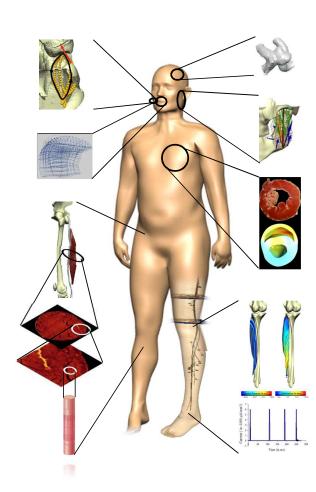
Simulation

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